

Figura 2.5

$$\mu_{\max} = \left(\frac{T}{F}\right)_{\max} = 0.87 \cdot \alpha \cdot \tau_0 + 1.74 \cdot \frac{\tau_0}{\overline{p}} \cdot \ln \left[\frac{1.2}{\tau_0 \cdot h} \cdot \frac{K \cdot \eta_a}{\beta \cdot (1+9.55)}\right]^{\frac{1}{2}}$$
(2.3)
$$n = \frac{P_u}{1 + 1.5} = \frac{T \cdot U_2}{1 + 1.5}$$
(2.4)

$$T = \frac{1}{P_u + P_{he} + P_{hl} + P_{rl}} - \frac{1}{T \cdot U_2 + P_{he} + P_{hl} + F_{rl} \cdot U}$$

$$T < F_r = \mu \cdot F;$$
(2.5)

$$T < F_{f} = \mu \cdot F; \quad \frac{2 \cdot M_{t1}}{D_{1}} < \mu \cdot F;$$
(2.6)

$$\frac{2 \cdot \beta \cdot M_{tl}}{D_1} = \mu \cdot F \tag{2.7}$$

Tabelul 2.1 m Cuplul de materiale Cu ungere Fara ungere Otel calit / otel calit 0,05 ... 0,06 0,15 ... 0,18 Otel / fonta 0,15 ... 0,20 -Textolit / otel; fonta cenusie 0,2 ... 0,25 _ 0,3 ... 0,35 Ferodo / otel -Cauciuc / fonta cenusie, otel 0,45 ... 0,85 $v_1 = \frac{\pi \cdot D_1 \cdot n_1}{60};$ $v_2 = \frac{\pi \cdot D_2 \cdot n_2}{60}$ (2.8) $i_{12} = \frac{n_1}{n_2} = \frac{D_2}{D_1}$ (2.9) $i_{12ef} = \frac{n_1}{n_2} = \xi \cdot \frac{D_2}{D_1}$ (2.10) $D_1 = (5 \dots 10) \cdot d_1$ (2.11) $B \ge \frac{F}{q_a}$, unde forta transmisa este $F = \frac{2 \cdot \beta \cdot M_{tl}}{\mu \cdot D_1}$. (2.12)

Tabelul 2.2

Cuplul de materiale	q _a [N/cm]	
Otel calit / otel calit	1500 2000	
Otel / fonta cenusie	1000 1500	
Textolit / otel; fonta cenusie	400 800	
Lemn / otel, fonta cenusie	100 150	
Lignofon / fonta cenusie, otel	400 600	
$\sigma_{H_{max}} = 0.418 \cdot \sqrt{\frac{F}{B} \cdot \frac{E}{\rho}}$	(2.13)	
$\frac{2}{E} = \frac{1}{E_1} + \frac{1}{E_2}$ si $\frac{1}{\rho} = \frac{2}{D_1} + \frac{2}{D_2}$	(2.14)	
$\sigma_{H \max} \leq \sigma_{H admisibil}$	(2.15)	

Tabelul 2.3

Cuplul de materiale	S _{H admisibil}
Otel necalit / otel necalit cu ungere	25 HB
Otel calit / otel calit cu ungere	30 HB
Textolit / otel neuns	50 80 MPa
β·Τ,	

$F' = F'_n \cdot (\sin \alpha + \mu \cdot \cos \alpha) Si F_n = \frac{1}{\mu} = z \cdot F_n$	(2.16)
$\mathbf{F}'=0,\mathbf{4F}$	(2.17)
$F' = F'_n \cdot \sin \alpha$	(2.18)
$\mathbf{F}' = 0, 26 \cdot \mathbf{F}$	(2.19)
$q = \frac{F_n \cdot \cos \alpha}{2 \cdot e} \le q_a$	(2.20)
$F_n = \frac{2 \cdot \beta \cdot M_{\iota 1}}{\mu \cdot d_{m1}}$	(2.21)
$F = F' \cdot z = F_n \cdot \sin \alpha \cdot z$	(2.22)

$$F = \frac{2 \cdot e \cdot q_a}{\cos \alpha} \cdot \sin \alpha \cdot z$$
(2.23)

$$F = 2 \cdot q_a \cdot e \cdot z \cdot tg\alpha$$
(2.24)

$$z_{\text{nec}} = \frac{F}{2 \cdot q_a \cdot e \cdot tg\alpha} \le 5...8$$

$$\sigma_{H_{max}} = 0.418 \cdot \sqrt{\frac{F_n}{2 \cdot B}} \cdot \frac{E_{red}}{\rho_{red}} \le \sigma_{H_{adm}}$$
(2.26)



$$i_{12} = \frac{n_1}{n_2} = \frac{D_{m2}}{D_{m1}} = \frac{\sin \delta_2}{\sin \delta_1} = \frac{1}{tg\delta_1}$$
$$i_{12ef} = \frac{1}{\xi} \cdot \frac{D_{m2}}{D}; \qquad \xi = 0.95...0.99$$

$$T_{12ef} = \xi D_{m1}$$
, $\zeta = 0,05...0,09$

$$F_{1} = F_{n} \cdot (\sin \delta_{1} + \mu \cdot \cos \delta_{1})$$

$$F_{2} = F_{n} \cdot (\sin \delta_{2} + \mu \cdot \cos \delta_{2})$$
(2.30)

$$F_{1} = F_{n} \cdot \sin \delta_{1}$$

$$F_{2} = F_{n} \cdot \sin \delta_{2}$$

$$F_{1} < F_{2}!$$

$$(2.31)$$

$$B \ge \frac{F_n}{q_a} = \frac{2 \cdot \beta \cdot M_{tl}}{\mu \cdot D_{ml} \cdot q_a}$$
(2.32)

$$F_1$$

 F_1
 F_1
 F_1
 F_2
 F_2

(2.25)

(2.27)

Caracteristica neliniara de reglaj Figura 2.11

(2.29)

$$\sigma_{H_{max}} = 0.418 \sqrt{\frac{F_n}{B} \cdot \frac{E_{red}}{\rho_{red}}} \le \sigma_{H_{ad}}$$

$$D_{m1}/2 \qquad D_{m2}/2$$
(2.33)

$$\rho_1 = \frac{D_{m1}/2}{\sin \delta_1}; \qquad \rho_2 = \frac{D_{m2}/2}{\sin \delta_2}$$
(2.34)

$$n_{2x} = n_1 \cdot \frac{r_{1x}}{R_2}$$
(2.35)

$$n_{2 \max} = n_1 \cdot \frac{(R_1 - B/2)}{R_2} \text{ si } n_{2\min} = n_1 \cdot \frac{B/2}{R_2}$$
 (2.36)

$$G = \frac{n_{2 \max}}{n_{2 \min}} = \frac{2 \cdot R_1 - B}{B} = \frac{2 \cdot R_1}{B} - 1$$
(2.37)

$$n_{2x} = n_1 \cdot \frac{R_2}{R_{1x}}$$
(2.38)

$$\frac{n_1}{n_3} = \frac{r}{R_{1x}} \text{ si } \frac{n_3}{n_{2x}} = \frac{R_{2x}}{r}$$
(2.39)

